



# DESIGN OF CONTAINER SHIP PROPULSION SYSTEM

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**Internship at ICEPRONAV Engineering S.R.L.**

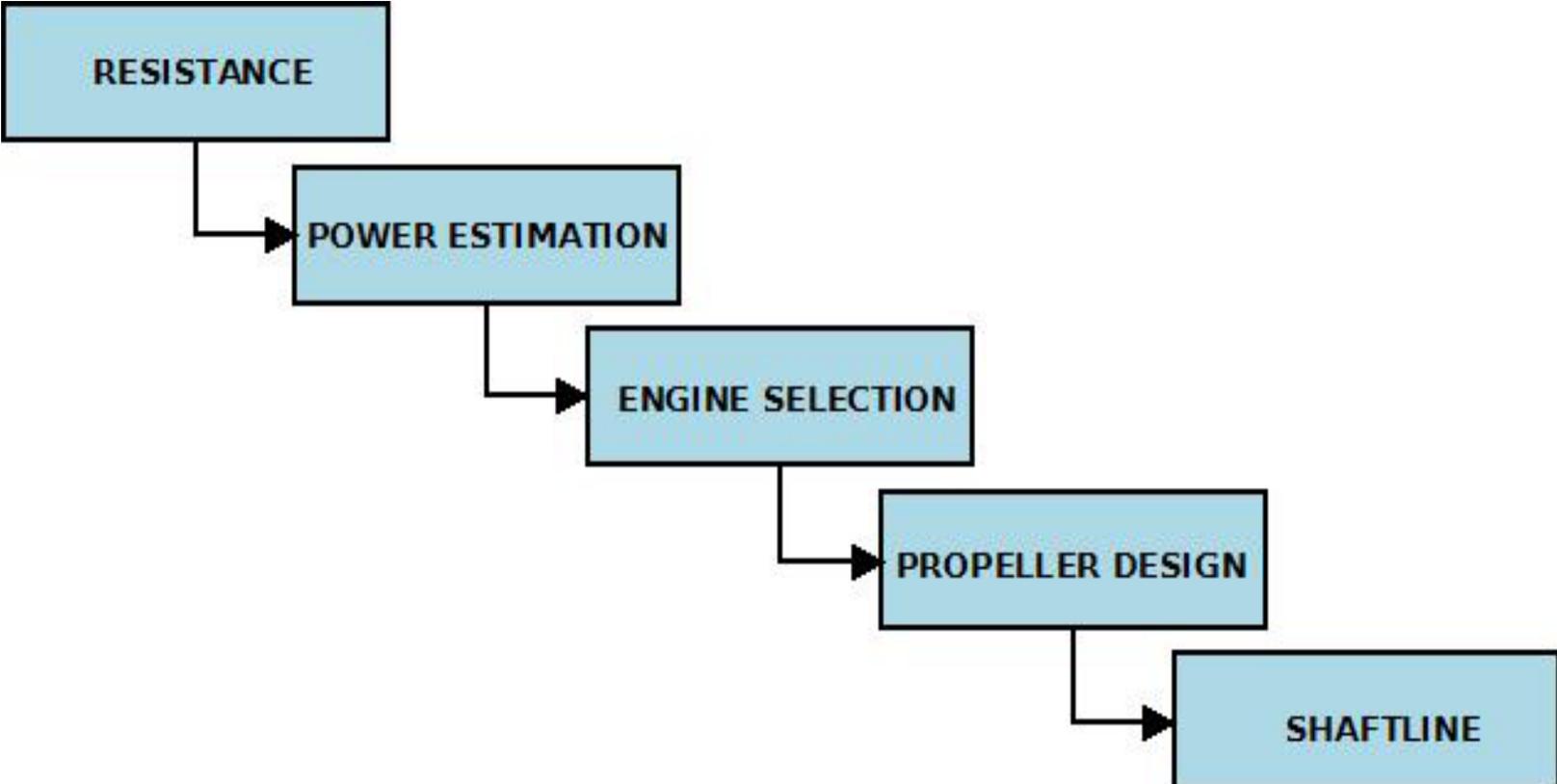
# INTRODUCTION



- The main purpose of this work was to design the propulsion system including Main Engine, an optimized Propeller and Transmission line for a Container ship with following characteristics.

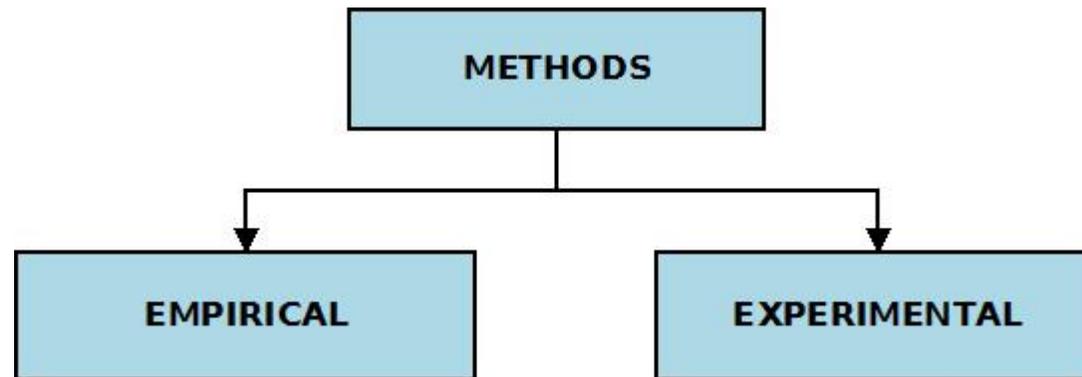
Particulars	Dimension
LENGTH BETWEEN PERPENDICULARS(M)	145.9
BREADTH(M)	23.25
DRAFT(M)	7.3
DEPTH(M)	11.5
SERVICE SPEED(KNOTS)	20
TEU	1200

# OBJECTIVES



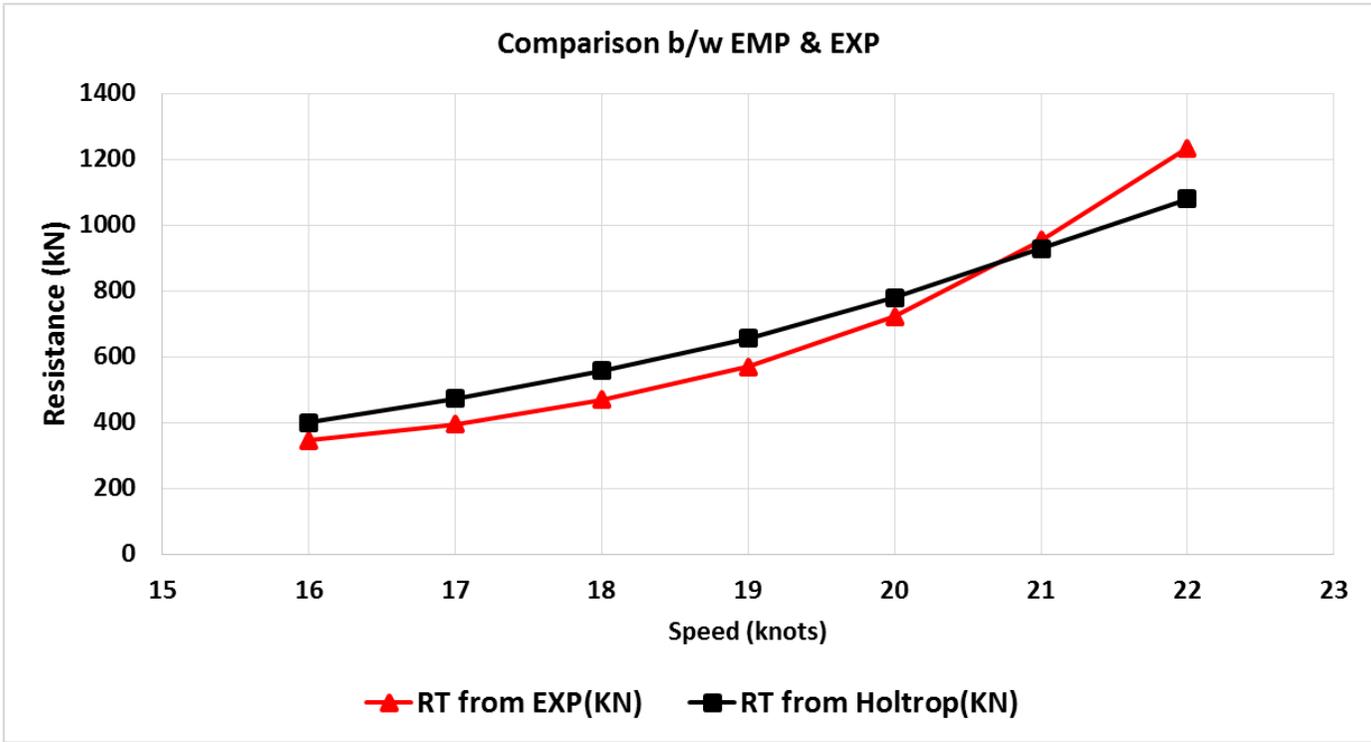
# RESISTANCE

- The opposing hydrodynamic fluid force experienced by the ship due to its motion.



- Resistance calculations were performed for a range of speeds from 16 to 22 Knots.

# RESULT COMPARISON



- The experimental method is more accurate compared to empirical methods.
- Hence the experimental result obtained as 722 KN at 20 knots has been used to start propeller design.

# POWER ESTIMATION

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The brake power of engine is influenced by

- Hull-Propeller interaction coefficients
- Hull, Relative rotative & Open water efficiencies.
- Sea and Engine margin as per owners requirement.

# POWER & OPTIMUM RPM



Propeller
- □ ×

INPUT		OUTPUT	
BAR	<input type="text" value="0.8"/>	Max Efficiency	<input type="text" value="0.670049"/>
No. of Blades	<input type="text" value="5"/>	Pitch Ratio	<input type="text" value="0.9"/>
Resistance(KN)	<input type="text" value="722"/>	Kt	<input type="text" value="0.188579"/>
wake Fraction	<input type="text" value="0.27"/>	Kq	<input type="text" value="0.0278423"/>
Thrust Fraction	<input type="text" value="0.2"/>	Advance Coeff	<input type="text" value="0.593566"/>
Diameter(m)	<input type="text" value="5.4"/>	Rot per Second	<input type="text" value="2.3433"/>
Speed(KN)	<input type="text" value="20"/>	Rot per Minute	<input type="text" value="140.598"/>
Density(t/m3)	<input type="text" value="1.025"/>	Thrust(KN)	<input type="text" value="902.503"/>
Viscosity	<input type="text" value="0.00000118"/>	Delivered Pow(KW)	<input type="text" value="10116.6"/>
Engine Mar(%)	<input type="text" value="10"/>	Hull Efficiency	<input type="text" value="1.09589"/>
Sea Margin(%)	<input type="text" value="15"/>	Behind Hull	<input type="text" value="0.68345"/>
Shaft Eff(%)	<input type="text" value="98"/>	Rotative Efficiency	<input type="text" value="1.02"/>
Gear Eff(%)	<input type="text" value="100"/>	QPC	<input type="text" value="0.748986"/>
No. of Prop	<input type="text" value="1"/>	Brake Power(KW)	<input type="text" value="13229.5"/>

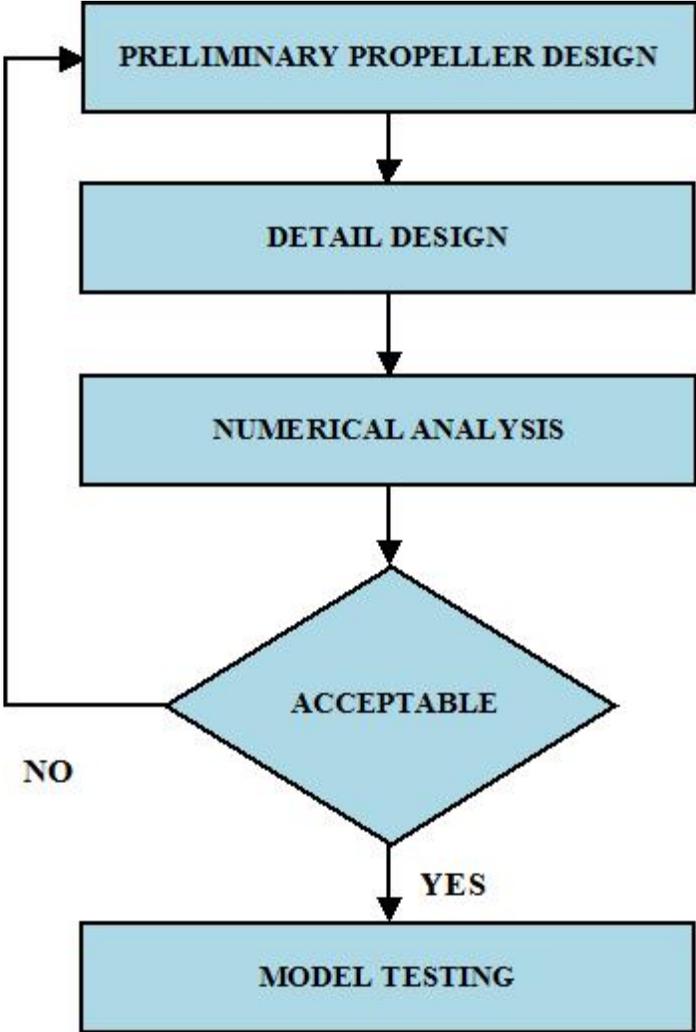
Kt vs J Diagram

# ENGINE SELECTION

- Low speed diesel engine has been selected as per the required brake power and RPM estimated.
- Main advantages include compatibility with inexpensive fuel and low maintenance.

ENGINE MANUFACTURER	MAN
MODEL	K60MC-S
NO.OF CYLINDERS	7
BRAKE POWER	13860 KW
RPM	150

# PROPELLER DESIGN



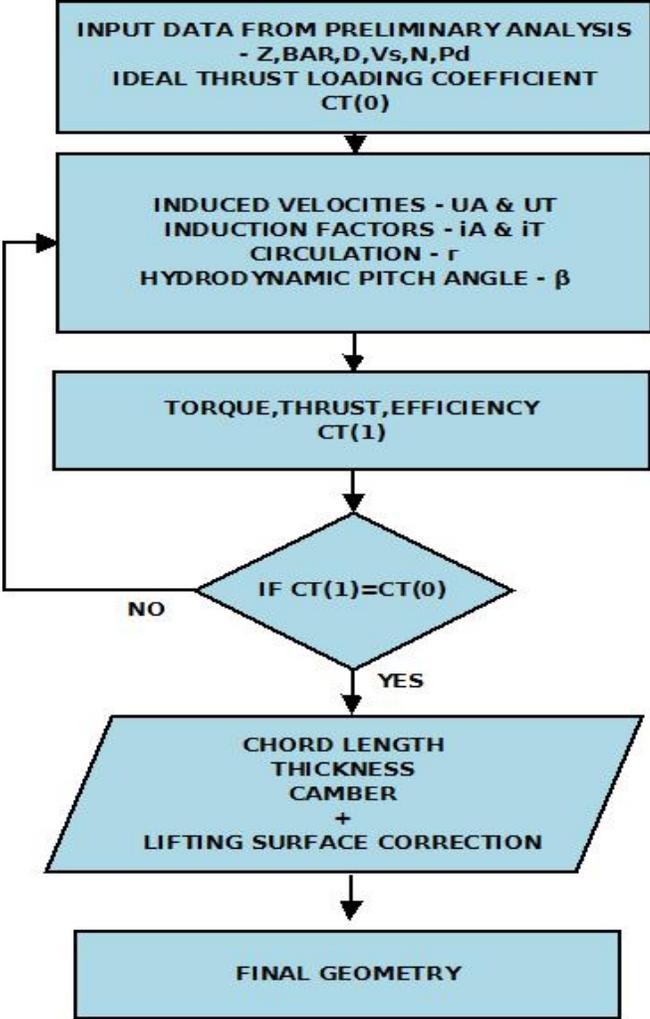
# PRELIMINARY DESIGN



**Propeller-Diameter**

INPUT	Kq vs J Diagram	OUTPUT
BAR <input style="width: 100%;" type="text" value="0.8"/>		Max Efficiency <input style="width: 100%;" type="text" value="0.663277"/>
No. of Blades <input style="width: 100%;" type="text" value="5"/>		Pitch Ratio <input style="width: 100%;" type="text" value="0.9"/>
Brake Power <input style="width: 100%;" type="text" value="13860"/>		Kt <input style="width: 100%;" type="text" value="0.192564"/>
wake Fraction <input style="width: 100%;" type="text" value="0.27"/>		Kq <input style="width: 100%;" type="text" value="0.0283296"/>
Thrust Fraction <input style="width: 100%;" type="text" value="0.2"/>		Advance Coeff <input style="width: 100%;" type="text" value="0.585477"/>
Engine RPM <input style="width: 100%;" type="text" value="150"/>		Diameter <input style="width: 100%;" type="text" value="5.31488"/>
Draft of Ship <input style="width: 100%;" type="text" value="7.3"/>		Torque <input style="width: 100%;" type="text" value="717.476"/>
Service Speed <input style="width: 100%;" type="text" value="20"/>		Hull Efficiency <input style="width: 100%;" type="text" value="1.09589"/>
Density <input style="width: 100%;" type="text" value="1.025"/>		Behind Hull <input style="width: 100%;" type="text" value="0.676542"/>
Viscosity <input style="width: 100%;" type="text" value="0.00000118"/>		Rotative Efficiency <input style="width: 100%;" type="text" value="1.02"/>
Engine Margin(%) <input style="width: 100%;" type="text" value="10"/>		QPC <input style="width: 100%;" type="text" value="0.741416"/>
Sea Margin(%) <input style="width: 100%;" type="text" value="15"/>		
Shaft Efficiency <input style="width: 100%;" type="text" value="98"/>		
Gear Efficiency <input style="width: 100%;" type="text" value="100"/>		

# DETAIL DESIGN



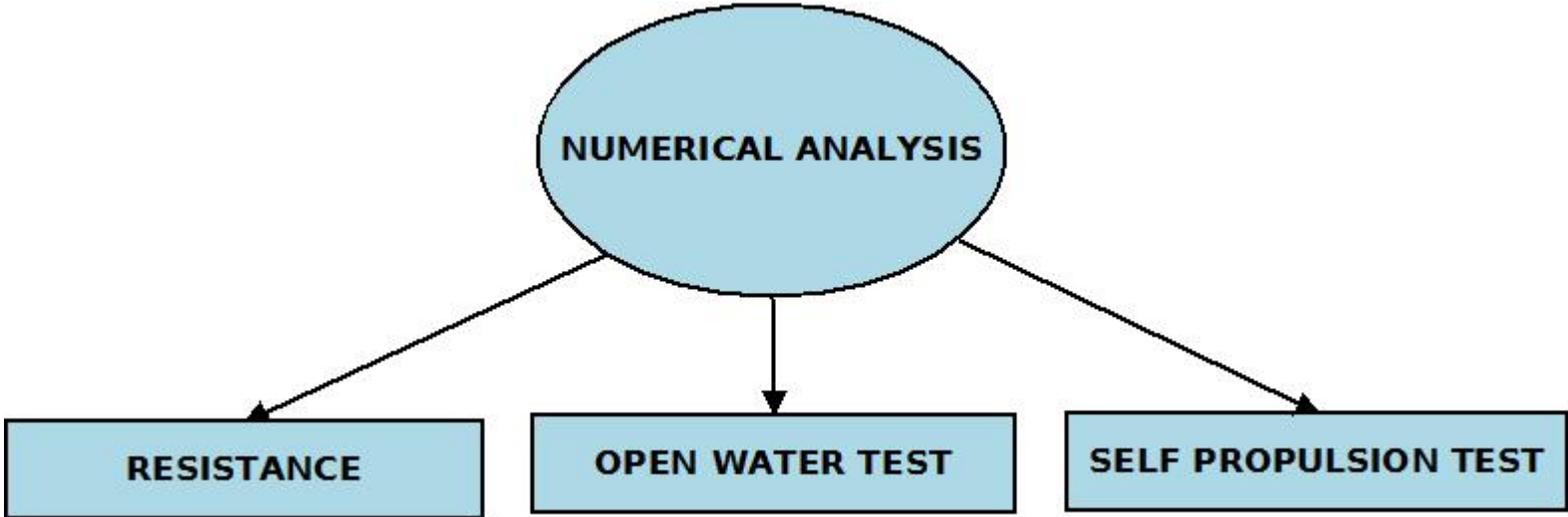
# PROPELLER CHARACTERISTICS



r/R	CHORD LENGTH (MM)	THICKNESS (MM)	CAMBER (MM)	PITCH (MM)
0.2	1454.6	255.5	0	3622.1
0.3	1609.9	218.9	82.3	4174.6
0.4	1749.3	185	54.3	4328.8
0.5	1866.7	152.9	43	4373
0.6	1952.1	123.5	34.4	4403.7
0.7	1987.1	95.8	28.8	4426.1
0.8	1933.8	69.4	24.8	4451.7
0.9	1685.5	44.7	22.2	4447
1	0	2.3	10.6	4443.7

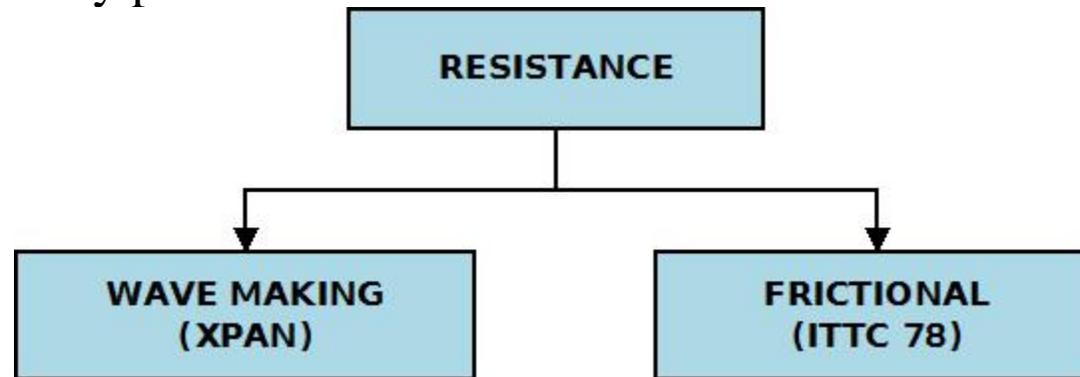
# NUMERICAL ANALYSIS

- To study hydrodynamic performance of propeller under steady as well as unsteady flow conditions.
- Helps to select a most promising candidate design for model testing to save time and cost.



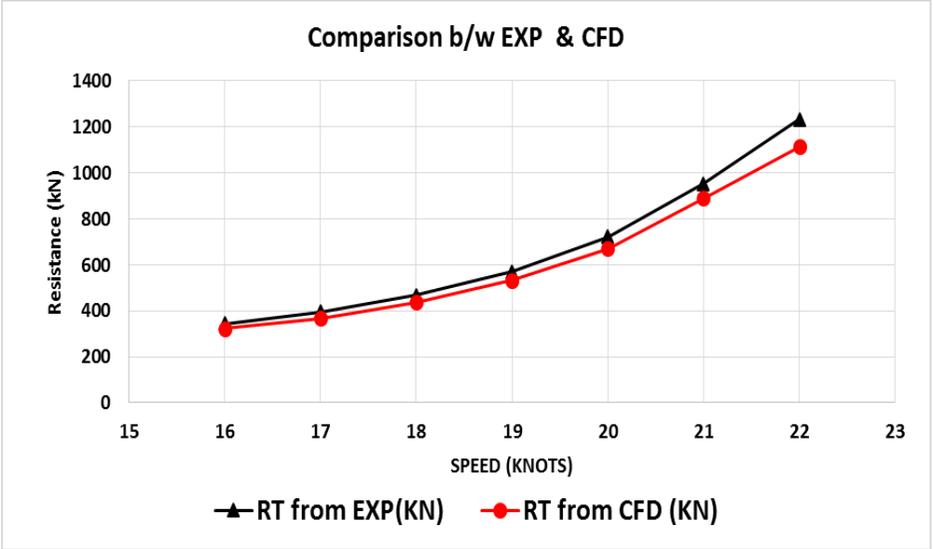
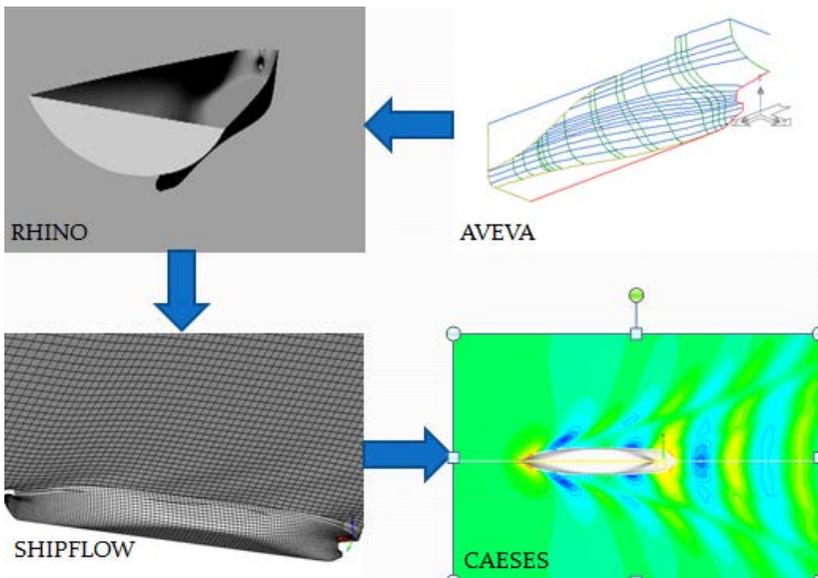
# RESISTANCE - CFD

- Resistance computation by potential flow solver of shipflow based on a surface singularity panel method.



- Discretization by automatic medium mesh generation mode to perform faster computation.(No of Panels – 6666)

# RESISTANCE - CFD



- The resistance data obtained from CFD method is in good agreement with experimental results.
- Result from CFD has been used during self-propulsion simulation.

# OPEN WATER TEST

- Simulation to study the propeller characteristics in steady flow.

## Pre – Processing

Structured Grid

Turbulence – EASM

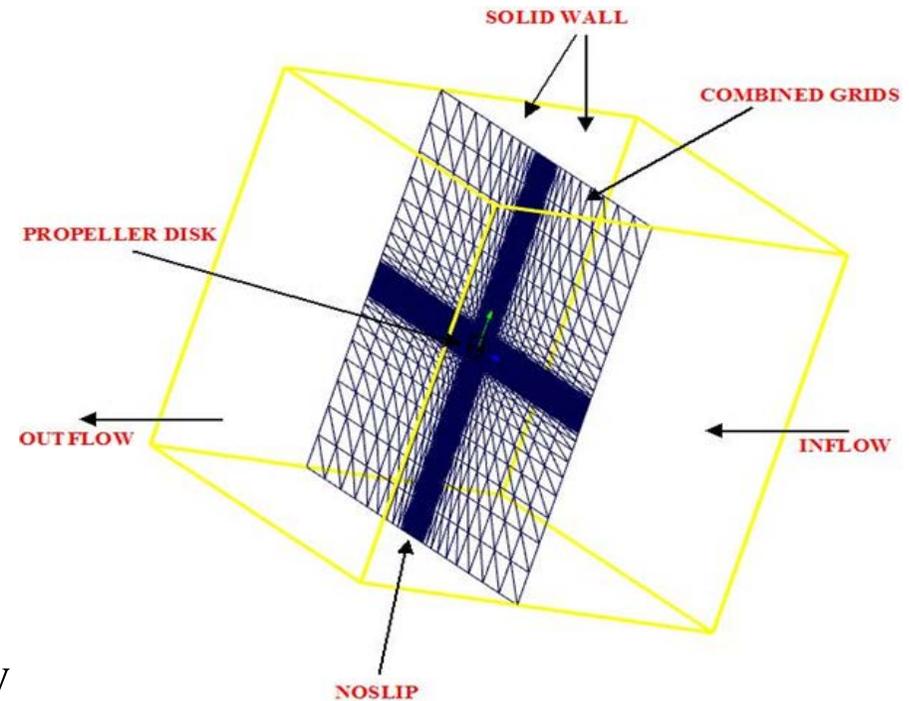
## Computation

RANSE solver – XCHAP

## Post – Processing

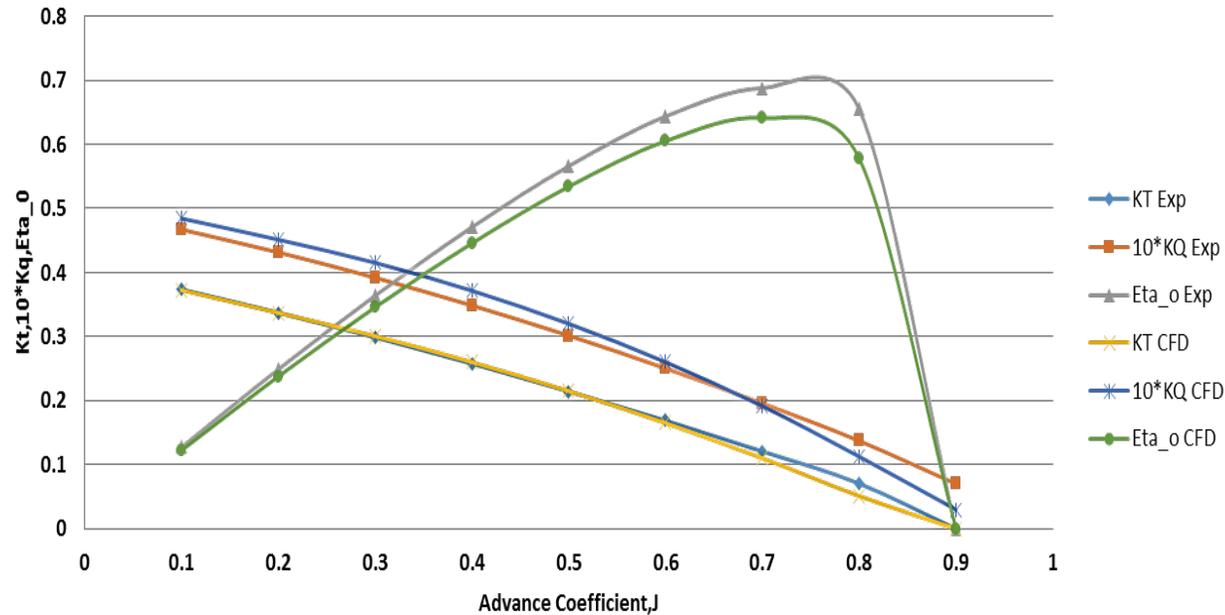
Propeller Characteristics

$K_t$ ,  $K_q$  and open water efficiency



# RESULT COMPARISON

Comparison b/w EXP & CFD



- Propeller characteristics obtained through CFD analysis are in good agreement with experimental results as it follows same pattern.
- Variations are within the range of 2-3%.

# SELF PROPULSION TEST

- The self-propulsion simulations were carried out to study the performance of propeller in non-uniform flow condition.

## Pre – Processing

Structured & Overlapping Grids

Turbulence – EASM

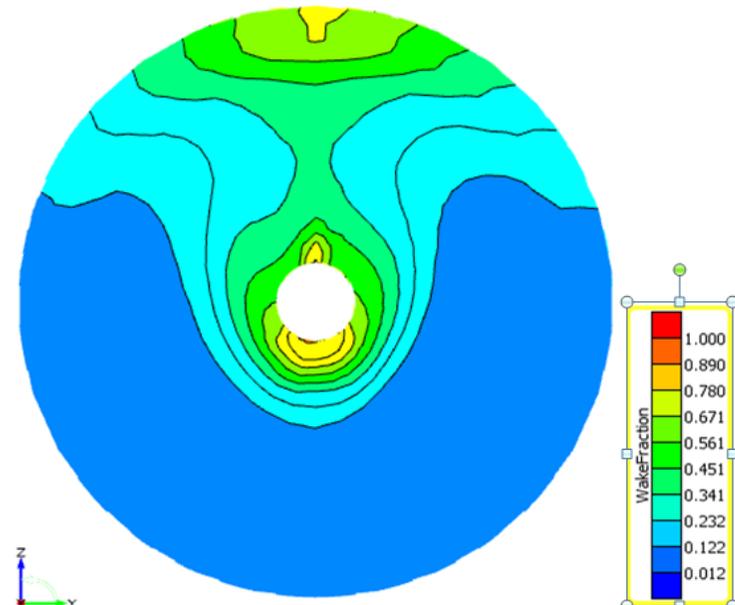
## Computation

RANSE solver – XCHAP

## Post – Processing

Wake, Propeller Characteristics,

Propeller Hull interactions, Delivered Power & RPM



# RESULT COMPARISON

PARAMETERS	NUMERICAL	EXPERIMENTAL	DIFFERENCE IN %
Effective Mean Wake, $w$	0.277	0.273	1.44
Thrust Deduction, $t$	0.18	0.1766	1.88
Resistance(KN)	649	722	10.11
Thrust Coefficient, $K_T$	0.178	0.177	0.5
Torque Coefficient, $K_Q$	0.0242	0.026	7.4
Propeller Speed (RPM)	141	144.16	2.24
Delivered Power (KW)	8234	10243.7	19.6
Hull efficiency, $\eta_H$	1.183	1.1326	4.2
Relative rotative eff, $\eta_R$	1.018	1.0225	4.2
Propeller Efficiency, $\eta_D$	0.71	0.73	2.8

# CONCLUSION

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- Preliminary design, detail design and numerical analysis of final propeller were carried out.
- Strength has been verified at 0.25R and 0.6R blade sections using classification rules.
- Numerical method have predicted efficiently the hull-propeller interaction factors  $w$ ,  $t$  & efficiencies ( $\eta_R, \eta_H, \eta_0$ ).  $K_t$  computed using CFD has a very reasonable accuracy while for  $K_q$  a larger deviation was observed.
- The wake adapted NACA propeller has been concluded as best available solution for containership with respect to its hydrodynamic performance.
- Finally a transmission system has been designed as per classification society requirement.